SMAQMD BACT CLEARINGHOUSE

CATEGORY Type: INCINERATOR/CREMATORY

MINOR SOURCE BACT Category:

232 **BACT Determination Number: BACT Determination Date:** 8/11/2020

Equipment Information

Permit Number: N/A -- Generic BACT Determination **CREMATORY - ANIMAL Equipment Description:**

Unit Size/Rating/Capacity: 4.5 MMBtu/hr

Equipment Location:

EXPIRED

BACT Determination Information

District Contact: Felix Trujillo Phone No.: (916) 874 - 7357 email: ftrujillo@airquality.org				
ROCs	Standard:	No Standard		
	Technology Description:	Natural gas fired and secondary combustion chamber (afterburner)=> 1600 F		
	Basis:	Achieved in Practice		
NOx	Standard:	60 ppm at 30% O2 or 0.073 lb/MMBtu		
	Technology Description:			
	Basis:	Achieved in Practice		
SOx	Standard:	No Standard		
	Technology Description:	Natural gas fired		
	Basis:	Achieved in Practice		
PM10 Standard: No Standard		No Standard		
	Technology Description:	Natural gas fired with secondary chamber operating at => 1600 F		
	Basis:	Achieved in Practice		
PM2.5	Standard:	No Standard		
Technology Description: Natural gas fired with secondary chamber operating at => 1600 F		Natural gas fired with secondary chamber operating at => 1600 F		
	Basis:	Achieved in Practice		
СО	Standard:	No Standard		
	Technology Description:	Secondary chamber => 1500 F		
	Basis:	Achieved in Practice		
LEAD	Standard:			
	Technology Description:			
	Basis:			

Comments: NOx standard is based on emissions from natural gas combustion only (not with the charge). BACT was based on a total burner rating of 4.5 MMBtu/hr operating at 4,380 hours/year (19,710 MMBtu/year) for natural gas combustion and a charge rate of 677 ton/year for the combustion of the animals. TBACT was determined to be equivalent to BACT.

Printed: 8/11/2020



BEST AVAILABLE CONTROL TECHNOLOGY & TOXIC BEST AVAILABLE CONTROL TECHNOLOGY DETERMINATION

	DETERMINATION NO.:	232
EXPIRED	DATE:	August 11, 2020
	ENGINEER:	Felix Trujillo, Jr.
Category/General Equip Description:	Pet Crematory	
Equipment Specific Description:	Pet Crematory	
Equipment Size/Rating:	Minor Source BACT;4.5 MMBtu/hr Burners @ 4,380 hours/year of operation (19,710 MMBtu/year) and ≤ 677 Tons Charge/year	
Previous BACT Det. No.:	145	

This new pet crematory BACT will update the previous pet crematory BACT No. 145. The previous BACT was based on a 400 lb/hr crematory with a combined burner rating of 4.5 MMBtu/hr (A/C 25091). Since the time of this last permitting action, this size of crematory has been the largest received for any new applications. Therefore, this BACT will be based on this size of crematory.

BACT ANALYSIS

A: ACHIEVED IN PRACTICE (Rule 202, §205.1a)

The following control technologies are currently employed as BACT for crematories.

US EPA

BACT Source: EPA/ RACT/BACT/LEAR Clearinghouse

Crematory		
voc	No Standard	
NOx	No Standard	
SOx	No Standard	
PM10	No Standard	
PM2.5	No Standard	
СО	No Standard	

Rule Requirements

None

CARB

BACT

Source: ARB BACT Clearinghouse

Crematory		
VOC	No Standard	
NOx	No Standard	
SOx	No Standard	
PM10	No Standard	
PM2.5	No Standard	
СО	No Standard	

Rule Requirements None

SMAQMD

BACT

SMAQMD BACT #145 (1/13/17)		
voc	No Standard, Natural gas-fired with secondary chamber operating at ≥1600 °F.	
NOx	60 ppm @ 3% O2 or 0.073 lb/MMBtu	
SOx	No Standard, Natural Gas Fired	
PM10	No Standard, Natural gas-fired with secondary chamber operating at ≥1600 °F	
PM2.5	No Standard	
СО	No Standard, Secondary Chamber ≥ 1500 °F	

Rule Requirements

Rule 419 - NOx from Miscellaneous Combustion Units (10/25/18)

New Crematories that are rated at 2 MMBTU/hr or greater located at a major source or greater than or equal to 5 MMBTU/hr located at an area source, must meet a standard of 60 ppmv corrected to 3% O2 for NOx and 400 ppmv corrected to 3% O2 for CO.

South Coast AQMD

BACT

From SCAQMD BACT Guidelines for Non Major Polluting Facilities, Page 38		
voc	No Standard, Natural Gas, Secondary Chamber ≥ 1500 °F	
NOx	60 ppm Compliance with Rule 1147	
SOx	No Standard, Natural Gas	
PM10	No Standard, Natural Gas, Secondary Chamber ≥ 1500 °F	
PM2.5	No Standard	
СО	No Standard	

Rule Requirements

Regulation XI, Rule 1147 - NOx Reductions from Miscellaneous Sources (7/7/17)

The purpose of this rule is to reduce nitrogen oxide emissions from gaseous and liquid fuel fired combustion equipment as defined in the rule. The rule requires that on or after January 1, 2010 any person owning or operating a unit subject to the rule shall not operate the unit in a manner that exceeds the applicable nitrogen oxide emission limits specified in table 1 at the time a District permit is required for operation of a new, relocated or modified unit. New, modified or relocated crematories fired at any temperature cannot exceed 60 ppm at $3\% O_2$ or 0.073 lb/MMBtu, Per Table 1 of this rule. A phone call to SCAQMD (Derek Hollinshead, 909-396-2275), permitting department confirmed that the NOx standard is for the burner operation only and not the cremation process (from BACT determination #133 – Human Crematory).

Requirements Table Rule 1147

Table 1 – NOx Emission Limit for Unit Heat Ratings	NOx Emission Limit PPM @ 3% O2, dry or Pound/mmBtu heat input		
325,000 Btu/hour	Process Temperature		
Gaseous Fuel-Fired Equipment	≤ 800° F	> 800 ° F and < 1200° F	≥ 1200 ° F
Crematory	60 ppm or 0.073 lb/mmBtu	60 ppm or 0.073 lb/mmBtu	60 ppm or 0.073 lb/mmBtu

San Diego County APCD

BACT

From SDCAPCD NSR Requirements for BACT		
voc	No Standard	
NOx	No Standard	
SOx	No Standard	
PM10	No Standard	
PM2.5	No Standard	
СО	No Standard	

Rule Requirements

None

Bay Area AQMD

BACT

From BAAQMD BACT Guideline (Document 53.1) – Crematory (9/12/07)			
VOC	No Standard, Secondary Combustion ≥ 1500 °F		
NOx	No Standard, Natural Gas Fired		
SOx	No Standard, Natural Gas Fired		
PM10	No Standard, Secondary Combustion ≥ 1600 °F (set Point at 1650 °F)		
PM2.5	No Standard		
СО	No Standard, Secondary Chamber ≥ 1500 °F		

Rule Requirements

None

San Joaquin Valley APCD

BACT

From S.	From SJVAPCD BACT Guidelines (1.9.3) – Crematory – Natural Gas Fired (6/1/05)		
voc	No Standard, Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1600 °F		
NOx	No Standard, Natural Gas Fuel		
SOx	No Standard, Natural Gas Fuel		
PM10	No Standard, Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1600 °F		
PM2.5	No Standard		
СО	No Standard		

Rule Requirements None

The following control technologies have been identified and are ranked based on stringency:

SUMMARY OF ACHIEVED IN PRACTICE CONTROL TECHNOLOGIES			
voc	 No Standard 1) Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1,600 °F, SMAQMD, SJVUAPCD 2) Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1,500 °F, SMAQMD, BAAQMD 		
NOx	60 ppm at 3% O2 or 0.073 lb/MMBTU measurement of the fuel burned only, SCAQMD, SMAQMD		
SOx	No Standard, Natural Gas Fuel.		
PM10	No Standard, 1) Natural gas-fired with secondary chamber operating at ≥1,600 °F SMAQMD, SJVAPCD, BAAQMD 2) Natural Gas, Secondary Chamber ≥ 1,500 °F, SCAQMD		
PM2.5	No Standard		
СО	No Standard, Secondary Chamber ≥ 1,500 °F, BAAQMD		

The following control technologies have been identified as the most stringent, achieved in practice control technologies:

BEST CONTROL TECHNOLOGIES ACHIEVED			
Pollutant	Standard	Source	
VOC	No Standard, Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1,600 °F	SMAQMD, SJVUAPCD	
NOx	60 ppm at 3% O2 or 0.073 lb/MMBTU	SCAQMD, SMAQMD	
SOx	No Standard, Natural Gas Fired	SCAQMD, SMAQMD, BAAQMD, SJVAPCD	
PM10	No Standard, Natural gas-fired with secondary chamber operating at ≥1600 °F	SMAQMD, SJVAPCD, BAAQMD	
PM2.5	No Standard		
СО	No Standard, Secondary Chamber ≥ 1,500 °F	BAAQMD	

B. TECHNOLOGICALLY FEASIBLE AND COST EFFECTIVE (Rule 202, §205.1.b.):

Technologically Feasible Alternatives:

Any alternative basic equipment, fuel, process, emission control device or technique, singly or in combination, determined to be technologically feasible and cost effective by the Air Pollution Control Officer.

Updated in 2005, the SJVAPCD lists the use of a baghouse with a dry scrubber or a wet scrubber as technologically feasible for the control of SOx, the use of a venturi scrubber for the control of PM10 and the use of selective catalytic reduction (SCR) or a low NOx burner for the control of NOx. The control strategies appear to be carryovers from other natural gas combustion operations and do not appear to be fully evaluated for a crematory. The BAAQMD evaluated the same source category in 2007 and do not list a baghouse, venturi scrubber, the use of an SCR or a low NOx burner as technologically feasible options. No other district lists these options as technologically feasible either. Additionally, SMAQMD contacted SJVAPCD (Manuel Salinas, 559-230-5833) and verified that a SCR, low NOx burner, baghouse or scrubber has not been installed on any crematories to date. Irrespective of the discussion above that questions San Joaquin's intent for listing add on controls as being technologically feasible for a crematory application, the following analysis will assume that add on controls are technologically feasible and a cost effectiveness determination needs to be conducted to determine if add on controls are in fact considered cost effective. The driving factor for this BACT determination is the multi-pollutant cost effectiveness thresholds for SOx and PM10 calculated below. The limiting factor was based on yearly cremation of 677 tons/year and assuming the 4.5 MMBtu/hr burners operate 12 hours/day and 365 days/year. The life of the equipment was based on the life recommended in the cost manual. The interest was based on the previous 6-month average interest rate on US Treasury Securities + 2 points and rounding up to the next integer rate. As of June 5, 2020, the 10 year treasure rate (as found on http://www.multpl.com/10-year-treasury-rate/table/by-month) for the last 6 months beginning in January 1, 2020 and ending in June 1, 2020 was 1.76%, 1.50%, 0.87%, 0.66%, 0.67, and 0.82%. The average is 1.04%. Two percentage points are then added to the average interest rate and the interest rate is then rounded up to the next higher integer rate. Therefore, the resultant annual interest rate to be used is 1.04% + 2% = 4%.

The labor costs were based on data from the Bureau of Labor Statistics (operating labor: Occupation Code 49-9099, maintenance labor: Occupation Code 51-9051).

NOx:

A cost effectiveness analysis was done to determine if an SCR system could be considered cost effective to control the NOx from a crematory and is calculated in Appendix A of this document. The crematory is estimated to have a burner that when fired only on natural gas with no body will emit NOx at less than 60 PPM. To estimate the NOx emissions attributed to the burning of the charge, AP-42 Chapter 2.3 - Medical Waste Incineration Table 2.3-1 was used. This value for NOx is 3.56 lb of NOx per ton of charge. The NOx emissions from natural gas combustion were based on the total burner rating of 4.5 MMBtu/hr and an operation time of 12 hours/day and 365 days/year. As a worst case assumption, and consistent with the crematory permitting manual of the BAAQMD, the NOx emission factor that is used in this analysis will be the combined emission factor of 5.68 lb of NOx/ton of charge which includes the emission factor of natural gas combustion added to the emission factor from burning of the charge.

The total charge would be 677 tons per year. With an SCR NOx control efficiency of 90%, the NOx emissions from the crematory is calculated to be 0.19 tons per year (677*5.68*(1-0.9)/2000=0.19).

A cost for a SCR system was estimated using EPA's Cost Control Manual, 6th Edition. The SCR sizing criteria for which the costs are based are primarily determined from the exhaust flow rate and temperature. The spreadsheet that was used determines the flow rate from the burner rating. However, a crematory unit's flow rate is much larger than the flow rate estimated from the burner rating alone as it is dependent on exhaust generated from natural gas combustion, exhaust generated from the charge itself, and additional excess air. As a result, the analysis will utilize the actual average flow rate observed during source testing of an identical crematory unit (see Attachment B) and a calculated equivalent burner rating.

The total annualized cost for the SCR system is estimated to be \$42,749.47. The total NOx controlled would be 1.73 tons per year (677*5.68*0.9/2000 = 1.73). The analysis shows the cost effectiveness calculation to be \$24,749.47 per ton of NOx reduced. Since the District's cost effectiveness threshold for NOx is \$24,500 per ton, the addition of the SCR would not be considered cost effective.

Total Annualized Cost of SCR	Quantity of NOx Controlled (TPY)	Cost of SCR per ton removed	SMAQMD cost effective threshold for NOx	Cost effective
\$42,822.85	1.73	\$24,749.47	\$24,500	No

PM:

A screening cost effectiveness analysis was done to determine if a baghouse could be considered cost effective to control the particulate from a crematory. This analysis will assume that the baghouse will collect 100% of the particulate emissions which would be approximately 1.65 tons/yr.

Based on EPA's Cost Control Manual, 6th Edition, the total annual cost of a baghouse needed to control the flow characteristics of a crematory is estimated to be approximately \$30,155.76. The total PM10 emissions controlled would be 1.65 tons/year. The analysis shows the cost effectiveness calculation to be \$18,276.22 per tons of PM10 reduced. Therefore, the conclusion is that a baghouse used to control particulate matter for a crematory is not considered cost effective and as such will not be considered BACT. See Appendix A for cost analysis.

Total Annualized Cost of a Baghouse	Quantity of PM10 Controlled (TPY)	Cost of a Baghouse per ton removed	SMAQMD cost effective threshold for PM10	Cost effective
\$30,155.76	1.65	\$18,276.22	\$11,400	No

A screening cost effective analysis was done for a venturi scrubber using the EPA Cost Control Manual, 6th Edition. The entire PM quantity (filterable and condensable) was used for cost effectiveness determination. A venturi scrubber system sized to control 3,341 cfm of

exhaust gas is estimated to cost \$55,050.82. The total annual cost is \$32,665.40. The total PM10 emissions controlled would be 1.65 tons/year. The analysis shows the cost effectiveness calculation to be \$19,630.65 per tons of PM10 reduced. Since the system costs are greater than the District's cost effectiveness criteria, a venturi scrubber is not considered cost effective.

Total Annualized Cost of Venturi Scrubber	Quantity of PM10 Controlled (TPY)	Cost of Venturi per ton removed	SMAQMD cost effective threshold for PM10	Cost effective
\$32,665.40	1.664	\$19,797.21	\$11,400	No

SOx:

A cost effectiveness analysis was done for the control of SOx with the use of a wet scrubber. Based on the information presented in the EPA Cost Control Manual, 6th Edition, the cost of the capital equipment was selected by using the lowest surface area and subsequent cost information available in this section of the manual. For SOx, the District's cost effectiveness threshold is \$18,300 per ton. The cost of the wet scrubber was estimated to have a total annual cost of \$32,464.21 and control efficiency was assumed to be 100%. The cost of the electricity was included. The cost of caustic was not considered. The total SOx emissions controlled is 0.74 tons/year. The cost per ton removed for this control was calculated to be \$43,870.55 and therefore is not considered to be cost effective.

Total nnualized Cost Wet Scrubber	Quantity of SOx Controlled (TPY)	Cost of wet scrubber per ton removed	SMAQMD cost effective threshold for Sox	Cost effective
\$32,464.21	0.74	\$43,870.55	\$18,300	No

The EPA Cost Control Manual, 6th Edition does not have a chapter on dry scrubbers. A dry scrubber consists of a dry reactant or powder injection system and a baghouse. Costs for a dry scrubber are estimated using the equipment costs of a baghouse. Since the reference manual does not have cost information for the powder injection system, powder storage silo and powder reactant. The cost of the blower fan for the injection system was assumed to be 1/3 the size of the fan of a wet scrubber in order to determine the annual costs of the electricity for this system. The cost of the storage silo and powder reactant were not included. The total annualized costs are estimated to be \$32,448.61. The cost per ton of SOx removed is calculated to be \$43,849.47 and therefore is not considered to be cost effective.

Total Annualized Cost of dry scrubber	Quantity of SOx Controlled (TPY)	Cost of dry scrubber per ton removed	SMAQMD cost effective threshold for SOx	Cost effective
\$32,448.61	0.74	\$43,849.47	\$18,300	No

PM + SOx:

Per the SMAQMD *Procedures for Making Best Available Control Technology (BACT) and Best Available Control Technology for Toxic (T-BACT) Determinations for New and Modified Emission Units (10/15)*, when a control technology is expected to control multiple forms of criteria pollutants both shall be assessed for cost effectiveness. In the case of a wet scrubber, the control of SOx, and PM10 should be considered. Per the calculation method found in the document, and assuming that 100% of PM10 and SOx is removed by the wet scrubber

Max Cost = \sum (Emissions Reduced * Cost Effectiveness Value) P = Each pollutant subject to BACT

Max Cost = (1.65 ton PM10/yr X 11,400/ton PM) + (0.74 ton SOx/yr X 18,300/ ton SOx)= \$32,352/yr

Since the annualized costs of a wet scrubber is \$32,464.21 or a dry scrubber with baghouse is \$32,448.61, and since either is greater than the Max Cost value calculated above, the use of a wet scrubber or dry scrubber with baghouse is not considered cost effective.

APC Device	Total Annualized Cost	Quantity of SOx & PM10 Controlled (TPY)	Aggregate Max Cost Threshold for SOx & PM10	Cost effective
Wet Scrubber	\$32,464.21	0.745 tons SOx 1.664 tons PM10	\$32,352	No
Dry Scrubber with Baghouse	\$32,448.61	0.745 tons SOx 1.664 tons PM10	\$32,352	No

C. SELECTION OF BACT:

No technologically feasible control technologies were found to be cost effective and therefore not selected. BACT will be standards that have been achieved in practice.

BACT Foi	r A Pet Crematory: 4.5 MMBtu/hr Burners @ 4,380 h (19,710 MMBtu/year) and ≤ 677 Tons Charge	
Pollutant	Standard	Source
VOC	No Standard, Natural gas fuel and a secondary combustion chamber (afterburner) ≥ 1,600 °F	SMAQMD, SJVUAPCD
NOx	60 ppm at 3% O2 or 0.073 lb/MMBTU, measured as emissions from the fuel burning, not with the charge	SCAQMD
SOx	No Standard, Natural Gas Fired	SCAQMD, SMAQMD, BAAQMD, SJVAPCD
PM10	No Standard, Natural gas-fired with secondary chamber operating at ≥ 1,600 °F	SMAQMD, SJVAPCD, BAAQMD
PM2.5	No Standard, Natural gas-fired with secondary chamber operating at ≥ 1,600 °F	SMAQMD, SJVAPCD, BAAQMD
СО	No Standard, Secondary Chamber ≥ 1,500 °F	BAAQMD

D. SELECTION OF T-BACT:

There are no Federal NSPS's, NESHAP's nor State ATCM's for this source category. None of the sources surveyed have any toxic T-BACT determinations published. The District contacted the SCAQMD, the BAAQMD and the SJVAPCD to enquire about any T-BACT determinations that may not have been published for this source category. In all cases, the T-BACT determinations were essentially the crematory's operational parameters that have been required as BACT. Therefore, T-BACT standards will be considered as meeting the BACT standards identified above.

APPROVED BY:	Brian F Krebs	DATE:	08/11/2020	
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Appendix A Cost Analysis

SCR COST EFFECTIVENESS CALCULATION

Reagent Solution Cost Catalyst Replacement

Annual Catalyst Replacement

EPA AIR POLLUTION CONTROL COST MANUAL, Sixth Edition, EPA/452/B-02-001, January 2002 Section 4.2 - NOx Post-Combustion, Chapter 2 - Selective Catalytic Reduction

Cost Effectiveness = \$ 24,749.47 \$/ton

Temperature at SR: Rinder 1646.F7 of ognes 1775										
Cementary Open Security Cementary Open S	Fauinment									
Cementry (specified price 10			4.952057895	mmBTU/hr						
Communic property indices										
SECURE STATE										
Tacid Capidly Fations										
Baseline Note (19th Park name 1,55 le place of cause pt. 15										
**Secretion Final Front AP-07 Tables 2-31 Medical wasser incornection										
Second 1.58-01 Mymarib 1.58-01 Mymar										
SET Note Of Sciented 1.588-00 Mymeth	*Nox emission Rate from AP-42 Table 2.3-1 Medical waste									
Amoninal Sign	incineration		1.58E-01	lb/mmBTU						
Ammon Schemerter Raho Stered Ra	SCR Nox (90% control)		1.58E-02	lb/mmBTU						
Seried Ammorial Scrieg days	Ammonia Slip		10	ppm						
Amonin Storage days	Ammonia Stochiometric Ratio		1.05							
Saline Content	Stored Ammonia Conc		29	%						
Persue drop for Sch Dathorsk Persue drop for sch Calalyst Laye Inche W.G. 1964 L67 degrees 104	Amonnia Storage days		90	days						
Pressure due for seck Catalyst Layer	Sulfur Content		0.005	%						
Total	Pressure drop for SCR Ductwork		3	inches W.G.			Rolling Acres	Test Results		
Septiment 1998 19	Pressure drop for each Catalyst Layer		1	inche W.G.			3/20/2013			AVE
Reginal multile	Temperature at SCR Inlet		1641.67	degrees F			1475	1675	1775	1641.6
Amual fareers falae	Cost year		1998							
Calabys took, praisement			20	years						
Calaby tool, replacement	Annual interest Rate		4	%						
Betting Power cot 1.1124 \$/RWh Ammonia Cot 1.0115 \$/RWh Ammonia Cot 1.0115 \$/RWh Catalyst Life 24000 hr Catalyst Life 240000 hr Catalyst	Catalyst cost, Initial		240	S/ft2						
Amona Cost 0.101 5/lb 24000 hr Catalyst Layers 2 full, 1 empty Frenctory Calculations 4.952057895 mm8TU/hr Gauga 3.952057895 mm8TU/hr Gauga 3.94 1 acfm 3.94 3.95 3.274 Rose 3.94 1 acfm 3.94 3.95 3.274 Rose 3.94 20057893 12 Rose 4.952057895 mm8TU/hr Gauga 3.4810078333 12 Rose 4.952057895 mm8TU/hr Gauga 3.4810078333 12 Rose 4.952057895 13 Rose 4.952057895 12			290	S/ft2						
Catalyst Line	Electrical Power cost		0.1124	\$/KWh						
Catalystayes	Ammonia Cost		0.101	\$/lb						
Cerematory Calculations	Catalyst Life		24000	hr						
Op/ Name 4,950,7895 mn8III/life Name 3314 acfm 203 378 24/2 SCR Reactor Calculations VOLUME 20,0873365 h3 Accessed 20,0873336 h3 Accessed Accessed 3,480208333 h2 Accessed 4,080239833 h2 Accessed 4,08023983 h12 Ac	Catalyst Layers	2 full, 1	empty							
Op/ Name 4,950,7895 mn8III/life Name 3314 acfm 203 378 24/2 SCR Reactor Calculations VOLUME 20,0873365 h3 Accessed 20,0873336 h3 Accessed Accessed 3,480208333 h2 Accessed 4,080239833 h2 Accessed 4,08023983 h12 Ac	Cramatory Calculations									
Quanta (1986) 3341 acfm 301 3736 3274 Nacco 0.9 0.9 SCR Reactor Calculations 252.0873365 113 3.480008338 112 Acasage 3.480008338 112 4.602239838 112 Ewel 2.000559817 ft 4.002239838 112 Inver 2.4 4.002239838 112 Inver 2.4 4.002249838 112 Inver 2.4 4.002239838 112 Invers 2.4 4.002239838 112 Invers 2.4 4.002239838 112 Invers 2.4 4.002239828 112 Invers 2.4 4.002239828 112 Invers 2.4 4.002239828 112 Invers 2.4 4.002239828 112 Inversion 2.2 2.2 In			4.052057905	mmDTII/hr						
Name							2012	2726	2274	224
SCR Reactor Calculations							3013	3/30	32/4	334
VO _{Catalog} 262,0873365 †ts Acaspe 3,480208333 †tz Acasp 4,002239583 ftz Inwe 2,00059817 ft Age 24 hare 4,137831026 Doza 25 boxs 287,4457757 ft Reagent Calculations Major 3,00084661 lb/hr mbg 1,048567798 lb/hr qu 0,140507742 gph Tank Volume 302,5672341 gal Cost Estimation Direct Costs 5 General Facilities 5 13,481,67 Engineering and home office fees 5 26,953.33 Process Contingency 5 13,481,67 Total Indirect Installation Costs 5 332,954.00 Total Plant Cost 5 332,954.00 Total Plant Cost 5 372,964.64 Inventory Capital 5 22,876 Total Capital Investment 5 3,596.47 Power 7,533464282 kW Power <t< td=""><td>INOX</td><td></td><td>0.3</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	INOX		0.3							
Ascard	SCR Reactor Calculations									
ACSIC ACSI	Vol _{Cetalyst}		262.0873365	ft3						
Asan Auguaria Aug	A _{Catalyst}		3.480208333	ft2						
F-We 2,00055981,7 ft A/4			4.002239583	ft2						
h _{mer} 4.137831026 h _{bER} 287.4457757 ft Reagent Calculations m _{taspint} 0.304084661 lb/hr m _{beg} 1.048567798 lb/hr q _{iss} 0.140077423 gph Tank Volume 302.567341 gal Cost Estimation Direct Costs DC \$ 269,633.34 Indirect Costs General Facilities \$ 13,481.67 Engineering and home office fees \$ 26,963.33 Process Contingency \$ 13,481.67 Total Indirect Installation Costs \$ 33,926.67 Project Contingency \$ 48,534.00 Total Plant Cost \$ 37,094.00 Preproduction Cost \$ 7,441.88 Inventory Capital \$ 29.8.76 Total Capital Investment \$ 379,764.64 Direct Annual Costs Maintenance Costs \$ 5,696.47 per yr Power 7.380364228 RW Annual Electricity \$ 7,240.40 per yr			2.000559817	ft						
hamer 4.137831026 Detail 25 hgad 287.445775 ft Reagent Calculations Present 0.304084661 lb/hr mbal 1.048567798 lb/hr qua 0.140007/423 gph Tank Volume 302.5672341 gal Cost Estimation Direct Costs DC \$ 269,633.34 Indirect Costs Seneral Facilites \$ 13,481.67 Engineering and home office fees \$ 26,963.33 Process Contingency \$ 13,481.67 Total Indirect Installation Cost \$ 5,3926.67 Project Contingency \$ 48,534.00 Total Plant Cost \$ 372,094.00 Preproduction Cost \$ 7,441.88 Inventory Capital \$ 328,76 Total Capital Investment \$ 379,764.64 Direct Annual Costs Maintenance Costs \$ 5,696.47 per yr Power 7.340.40 per yr	n _{lawar}		24							
Process			4.137831026							
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Annual Electricity \$ 7,240.40 per yr		>								
		ć								
Dealer Stroman III	Reagent Solution Cost	3								

927.73 per yr

1,014.51 per yr

0.320348539

5

Total Variable Direct Cost	\$ 9,182.64	per yr
Total Direct Annual Cost	\$ 14,879.11	per yr
CRF	0.07358175	
Indirect Annual Cost	\$ 27,943.75	per yr
Total annual Cost	\$ 42,822.85	peryr
NOx Removed	1.73	tons per year
Cost of NOx controlled per ton removal	\$ 24,749.47	per ton

3.56	NOx lb/ton(A)	400 lb/hr (B)
	(A) - Table 2.3-1 AP-42,	
	2.3 Medical Waste	(B) Burn rate of the crematory
	Incineration	
2.12	NOx lb/ton (C)	
	(C) - Natural gas combu	istion at 60 ppm
5.68	Combined NOx lb/ton	
	Ib of NOx based on	
tons of charge based on yearly limitation to remain below the cost	3.56 lb of NOx/ ton of	
effectiveness threshold for NOx.	charge	LB of NOx controlled based on 90%
677 tons	1.92 tons	1.73 tons

PM10 Baghouse Cost Effective Requirements

PM Cost effective Number 11400 \$/ton
PM emission from Crematory 1.65 tons/yer

CRF (4% interest and 20 year life) 0.07358175

Particulate Matter Control (Bag House) Cost Analysis

Gas to cloth ratio for shaker or reverse air bag house 1.8
A 9
B 0.8
L 0.1
D (mass mean diameter of particle, 7 um guess) 7

 V
 4.958928378 equation 1.11

 acfm of system
 3341 acfm

 Bag Size
 673.7342719 ft^2

 Cost of Bag house common housing design
 \$ 7,132.96 \$

 Cost of insulation
 \$ 2,543.43 \$

Cost of BAG Nextel, bottom bag removal \$ 11,231.15 high Temp Bags

Bag house cages 50.20 cage cost 12.23 \$/cage

Total cage costs \$ 613.96 \$ Equipment Costs (A) \$ 21,521.50

 Instrumentation
 \$ - 0*A

 California Sales taxes
 \$ 1,829.33
 0.085*A

 Freight
 \$ 1,076.08
 0.05*A

Purchase Equipment Cost (PEC) \$ 24,426.90

Direct & Indirect Installation Costs (DC & IC) \$ 4,885.38 0.2*PEC

Total Capital Investment (TCI) \$29,312.28

Direct Annual Costs

Operating Labor \$4,073.40 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$14.88

Supervisor \$611.01 15% of operating Labor

Maintenance Labor \$4,864.54 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$17.77

Material \$4,864.54 100% of maintenance labor

Electricity \$3,764.83 (0.000181)(3341 acfm)(10.3 in H2O)(4380 hr/yr)(\$0.138 kW/h)

Total Annual DC \$ 18,178.32

Indirect Annual Costs

Overhead \$8,648.09 60% of total labor and material

 Admin charges
 \$586.25
 2% of TCI

 Property Tax
 \$293.12
 1% of TCI

 Insurance
 \$293.12
 1% of TCI

Capital Recovery \$2,156.85
Total Annual IC \$11,977.43

Total Annal Costs (DAC + DIC) \$30,155.76

TAC/tons controlled \$18,276.22

PM10 Venturi Cost Effecive Analysis

Total PM 1.65 Tons/year
PM Cost effectiveness 11400 \$/tons controlled

CRF (4% interest and 15 year life) 0.0899411

From Table 2.8 Direct and Indirect Installation Costs for Venturi Scrubbers, EPA Control Cost Manual 6th edition, 1-02

Ventur Packaged Unit (A1) \$14,107.89 150*Q(sat)^0.56 3341 acfm low energy cabon

\$10,087.85 0.35*PEC

Additional Equipment (A2) \$11,286.31 80% of Unit Equipment Costs (A) \$25,394.20 A=A1 + A2

Instrumentation (assumed to be included per

 Section 6, Ch. 2, Table 2.5)
 \$0.00
 0*A

 California Sales taxes
 \$2,158.51
 0.085*A

 Freight
 \$1,269.71
 0.05*A

 Purchase Equipment Cost (PEC)
 \$28,822.42

Direct Installation Costs, DC \$16,140.56 0.56*PEC

Direct Annual Costs:

Total Indirect Costs, IC

Total Capital Investment (TCI)

Operating Labor \$4,073.40 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$14.88

\$55,050.82

Supervisor \$611.01 15% of operating Labor

Electricity \$6,310.23 (0.7457)(13 hp + 1 hp)(4380 hr/yr)(\$0.138 kW/h)

Maintenance Labor \$4,864.54 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$17.77

Material \$4,864.54 100% of maintenance labor

Total Annual DC \$20,723.72

Indirect Annual Costs:

Overhead \$5,837,45 60% of total labor and material

 Admin charges
 \$576.45
 2% of TCI

 Property Tax
 \$288.22
 1% of TCI

 Insurance
 \$288.22
 1% of TCI

Capital Recovery \$4,951.33 Total IAC \$11,941.68

Total Annual Costs (DAC +IAC) \$32,665.40

Cost Effectiveness \$19,797.21 \$/Ton Controlled

Cost Effective Requirements SOx Dry Scrubber

SOx Cost effective Number 18300 \$/ton SOx emissions 0.74 tons/yer

CRF (4% interest and 15 year life) 0.0899411

SOx Control (Bag House) Cost Analysis

Gas to cloth ratio for shaker or reverse air bag house 1.8
A 9
B 0.8
L 0.1
D (mass mean diameter of particle, 7 um guess) 7

 V
 4.958928378 equation 1.11

 acfm of system
 3341 acfm

 Bag Size
 673.7342719 ft^2

 Cost of Bag house common housing design
 \$7,132.96 \$

Cost of Bag house common housing design \$7,132.96 \$ Cost of insulation \$2,543.43 \$

Cost of BAG Nextel, bottom bag removal \$11,231.15 high Temp Bags

 Bag house cages
 50.20

 cage cost
 12.23 \$/cage

 Total cage costs
 \$613.96 \$

 Equipment Costs (A)
 \$21,521.50

 Instrumentation
 \$0.00 0*A

 California Sales taxes
 \$1,829.33 0.085*A

 Freight
 \$1,076.08 0.05*A

Purchase Equipment Cost (PEC) \$24,426.90

Direct & Indirect Installation Costs (DC & IC) \$4,885.38 0.2*PEC

Total Capital Investment (TCI) \$29,312.28

Direct Annual Costs

Operating Labor \$ 4,073.40 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$14.88

Supervisor \$ 611.01 15% of operating Labor

Maintenance Labor \$ 4,864.54 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$17.77

Material \$ 4,864.54 100% of maintenance labor

Electricity Baghouse \$ 3,764.83 (0.000181)(3341 acfm)(10.3 in H2O)(4380 hr/yr)(\$0.138 kW/h)

Electricity Dry Injection Blower \$ 1,813.32 (3 kW)(4380 hr/yr)(\$0.138 kWh)

Total Annual DC \$ 19,991.64

Indirect Annual Costs

Overhead \$ 8,648.09 60% of total labor and material

 Admin charges
 \$ 586.25
 2% of TCI

 Property Tax
 \$ 293.12
 1% of TCI

 Insurance
 \$ 293.12
 1% of TCI

 Capital Recovery
 \$ 2,636.38

 Total Annual IC
 \$ 12,456.96

Total Annal Costs (DAC + DIC) \$ 32,448.61

TAC/tons controlled \$ 43,849.47

Cost Effective Requirements SOx Wet Scrubber

SOx Cost effective Number 18300 \$/ton SOx emissions 0.74 tons/yer

CRF (4% interest and 15 year life) 0.0899411

Figure 1.4 pg 1-27, Setion 5.2 Post Combstion Controls, Chapter 1 Wet Scrubbers for

SOx Control (Packed Tower) Cost Analysis Acid Gas

Total Capital Investment

Equation 1.40 pg 1-24, Setion 5.2 Post Combstion Controls, Chapter 1 Wet Scrubbers for

Tower Cost \$ 7,935.00 69 ft^2 Acid Gas

Packing Costs \$ 207.00

AUX Eq (fan & Pump) \$ 4,071.00 1/2 the tower costs Guess

Euipment Costs (A) \$ 12,213.00

Instrumentation (assumed to be included per Section 6,

 Ch. 2, Table 2.5)
 \$0.00 0*A

 California Sales taxes
 \$ 1,038.11 0.085*A

 Freight
 \$ 610.65 0.05*A

Purchase Equipment Cost (PEC) \$ 13,861.76

DC \$ 11,782.49 0.85*PEC IC \$ 4,851.61 0.35*PEC

Total Capital Investment (TCI) \$ 30,495.86

Table 1.4, pg 1-28, Setion 5.2 Post Combstion Controls, Chapter 1 Wet Scrubbers for

 Direct Annual Costs
 Acid Gas

 Operating Labor
 \$ 4,073.40 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$14.88

Supervisor \$ 611.01 15% of operating Labor

Solvent (water)

Caustic replacement

Watewater disposal

Maintenance Labor \$ 4,864.54 (.5 hr/shift) (1 shift/8 hrs)(4380 hrs/yr)*\$17.77

Material \$ 4,864.54 100% of maintenance labor Electricity \$ 5,439.96 (9 kW)(4380 hr/yr)(\$0.138 kWh)

Total AC \$ 19,853.45

Indirect Annual costs

Overhead \$ 8,648.09 60% of total labor and material costs

 Admin charges
 \$ 609.92
 2% of TCI

 Property Tax
 \$ 304.96
 1% of TCI

 Insurance
 \$ 304.96
 1% of TCI

 Capital Recovery
 \$ 2,742.83

 Total IC
 \$ 12,610.76

Total annual costs (DC + IC) \$ 32,464.21

TAC/Ton of SOx controlled \$ 43,870.55

Appendix B Crematory Potential to Emit

Rating: 4500 cf					
400 lb/hr					
24 hr/day					
19,170,000 cf/year (equivalent to 19,170 MMI	3tu/yea				
677 tons charge/year					
Emission Maximum Allowable Emissi	one				
Pollutant Factor Maximum Allowable Emissi	UIIS				
(lb/MMcf) (lb/day) (lb/quarter) (lb/	(lb/year)				
VOC 5.4 0	104				
NOx 73 7.9 725	1399				
SOx 0.6 0.1 6	12				
PM10 7.5 0.8 75	144				
PM2.5 7.5 0.8 75	144				
CO 82.4 8.9 819	1580				
Emission Mayimum Allawahla Emissi	Marrian Allamatta Foriation				
Pollutant Factor Maximum Allowable Emissi	ons				
(lb/ton) (lb/day) (lb/quarter) (lb/	year)				
VOC 0.299 1.4 132 2	202				
NOx 3.56 17.1 1572 2	410				
SOx 2.17 10.4 958 1	469				
PM10 4.67 22.4 2062 3	162				
PM2.5 4.67 22.4 2062 3	162				
CO 2.95 14.2 1303 15	997				
Combined:					
Pollutant Maximum Allowable Emissions					
(lb/day) (lb/quarter) (lb/year) (ton/	year)				
VOC 1.4 132 306	0.15				
NOx 25.0 2297 3810	1.90				
004 4404	0.74				
SOx 10.5 964 1481	0.74				
PM10 23.2 2137 3305					
	1.65				

Appendix C Rolling Acres Memorial Garden for Pets Test

Source Emissions Report

Prepared for:

Rolling Acres Memorial Garden for Pets

12200 North Crooked Road Kansas City, MO 64152 Permit #: 112009-005

By:

Air Analysis Group, Inc. 17 E. Monroe St. #179 Chicago, IL 60603

(618) 394-1400

April 15, 2013

METHOD 5 - DETERMINATION OF PARTICULATE EMISSIONS - RESULTS

Plant Name	Rolling Acres Memorial Gardens	Date	03/20/13
Sampling Location	Kanasas City, MO	Project #	
Operator	Joe Nasseri	Stack Type	Circular

		Historica	I Data			
Run Number		R-1	R-2	R-3	Average	
Run Start Time		13:00	16:00	18:25		hh:mm
Run Stop Time		14:25	17:05	19:38		hh:mm
Meter Calibration Factor	(Y)	0.969	0.969	0.969		
Pitot Tube Coefficient	(C _p)	0.840	0.840	0.840		
Actual Nozzle Diameter	(D _{na})	0.490	0.490	0.580		in
		Stack Tes				
Initial Meter Volume	(V _m) _i	321.980	354.590	391.325		ft ³
Final Meter Volume	$(V_m)_f$	354.490	391.100	423.800		ft ³
Total Meter Volume	(V _m)	32.510	36.510	32.475	33.832	ft ³
Total Sampling Time	(□)	60.0	60.0	60.0	60.0	min
Average Meter Temperature	(t _m) _{avg}	51.0	56.8	70.4	59.4	°F
Average Stack Temperature	$(t_s)_{avg}$	814.3	1244.1	1493.5	1184.0	°F
Barometric Pressure	(P _b)	29.45	29.45	29.45	29.45	in Hg
Stack Static Pressure	(P _{static})	-0.09	-0.09	-0.09	-0.09	in H ₂ O
Absolute Stack Pressure	(P _s)	29.44	29.44	29.44	29.44	in Hg
Average Orifice Pressure Drop	(□H) _{avg}	1.10	1.36	1.02	1.16	in H ₂ O
Absolute Meter Pressure	(P _m)	29.53	29.55	29.52	29.54	in Hg
Avg Square Root Pitot Pressure	(□p ^{1/2}) _{avg}	0.23	0.25	0.21	0.23	(in H ₂ O) ^{1/2}
		Moisture Con	tent Data			
Impingers Water Volume Gain	(V _n)	81.0	139.0	115.0	111.7	ml
Impinger Weight Gain	(W _n)	7.1	8.0	7.1	7.4	g
Total Water Volume Collected	(V _{Ic})	88.1	147.0	122.1	119.1	ml
Standard Water Vapor Volume	$(V_w)_{std}$	4.147	6.920	5.748	5.605	scf
Standard Meter Volume	$(V_m)_{std}$	32.127	35.699	30.915	32.914	dscf
Calculated Stack Moisture	(B _{ws(calc)})	11.4	16.2	15.7	14.4	%
Saturated Stack Moisture	$(B_{ws(svp)})$	100.00	100.0	100.0	100.0	%
Reported Stack Moisture Content	(B _{ws})	11.4	16.2	15.7	14.4	%
		Gas Analys				
Carbon Dioxide Percentage	(%CO ₂)	6.0	7.9	10.2	8.0	%
Oxygen Percentage	(%O ₂)	11.7	10.1	7.1	9.7	%
Carbon Monoxide Percentage	(%CO)	0.0	0.0	0.0	0.0	%
Dry Gas Molecular Weight	(M _d)	29.43	29.67	29.91	29.67	lb/lb-mole
Wet Stack Gas Molecular Weight	(M _s)	28.12	27.77	28.05	27.98	lb/lb-mole
Volumetric Flow Rate Data						
Average Stack Gas Velocity	(v _s)	20.87	25.89	22.69	23.15	ft/sec
Stack Cross-Sectional Area	(A _s)	2.41	2.41	2.41		ft ²
Actual Stack Flow Rate	(Q _{aw})	3013	3736	3274	3341	acfm
Wet Standard Stack Flow Rate	(Q _{sw})	74	68	52	65	wkscfh
Dry Standard Stack Flow Rate	(Q _{sd})	1088	954	734	925	dscfm
Percent of Isokinetic Rate	(I)	90.4	114.5	92.0	99.0	%
Mass of Particulate on Filter	(m)	7.750000000		07.750000000	47 400000555	
Mass of Particulate in Acetone	(m _f)		16.700000000	27.750000000	17.400000000	mg
Mass due to Acetone Blank	(m _a ')	7.700000000	5.300000000	10.300000000	7.766666667	mg
	(W _a)	0.00000	0.00000	0.00000	0.00000	mg
Total Mass of Particulates Stack Particulate Concentration	(m _n)	15.450000000	22.000000000	38.050000000	25.166666667	mg
Stack Farticulate Concentration	(c _s)	0.000480905	0.000616260	0.001230789	0.000775985	g/dscf
Particulate Emission Deta	(C _s)	0.007421505	0.009510357	0.018993996	0.011975286	gr/dscf
Particulate Emission Rate	(E)	0.031390842	0.035281900	0.054233220	0.040301987	kg/hr
L	(E)	0.069205017	0.077783338	0.119563881	0.088850745	lbs/hr

FACILITY DESCRIPTION

The facility tested is an Animal Incinerator. This plant includes the following equipment:

EQUIPMENT	MANUFACTURED BY	MODEL	
Incinerator	Matthews	IEB Series 56	

The fuel used for the incinerator during testing was natural gas.

PROCESS OPERATION

On March 20, 2013, the following process data was recorded by the plant operators:

TEST RUN	BURN TEMPERATURE	TEMPERATURE AT THE	AVERAGE
NUMBER	AT START (⁰ F)	END (^o F)	TEMPERATURE (^o F)
Run 1	1400	1550	1475
Run 2	1675	1675	1675
Run 3	1775	1775	1775

The weight processed was approximately 2,488 pounds.